



# Magnet Basics

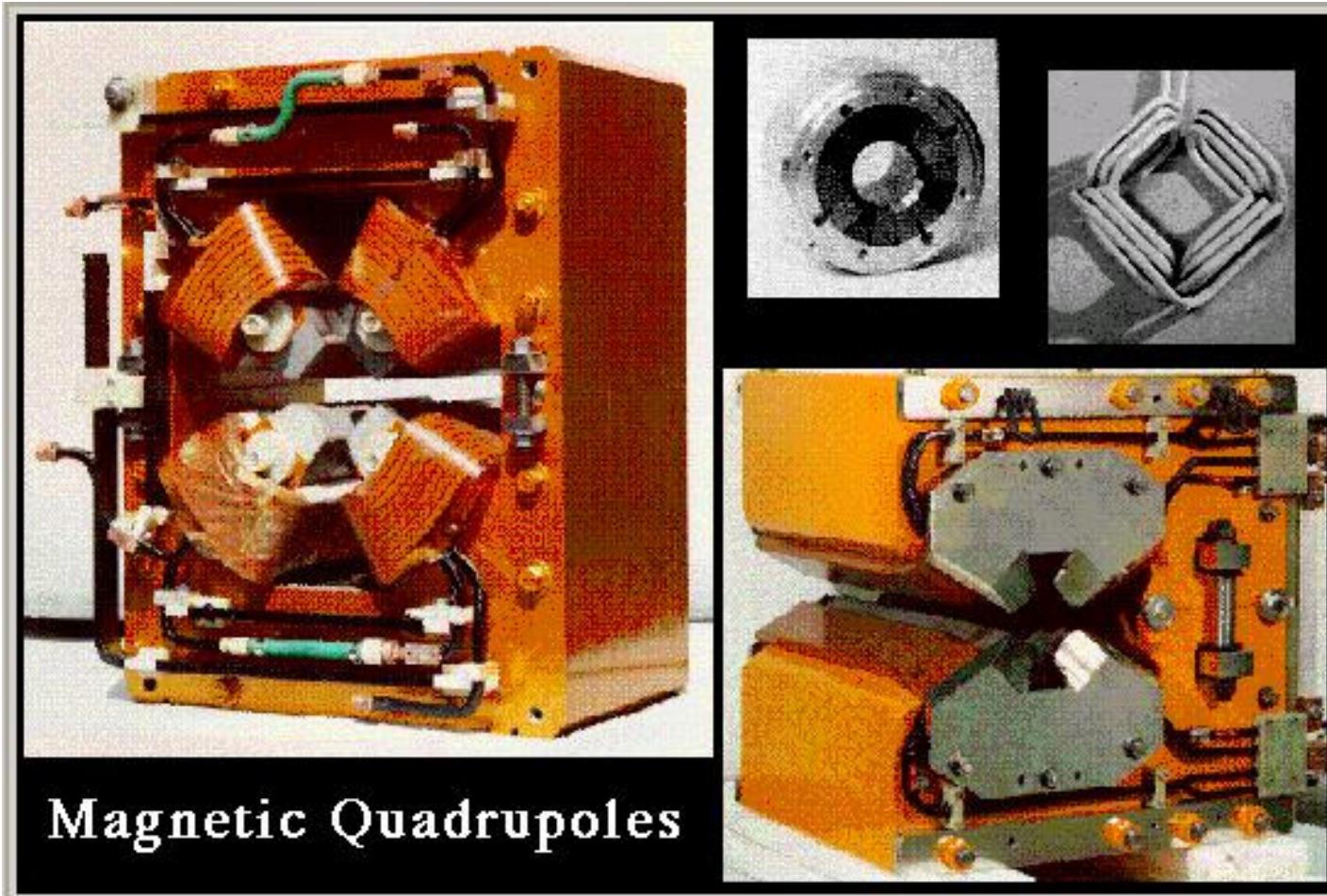
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**USPAS 08**  
**U. of Maryland, College Park**

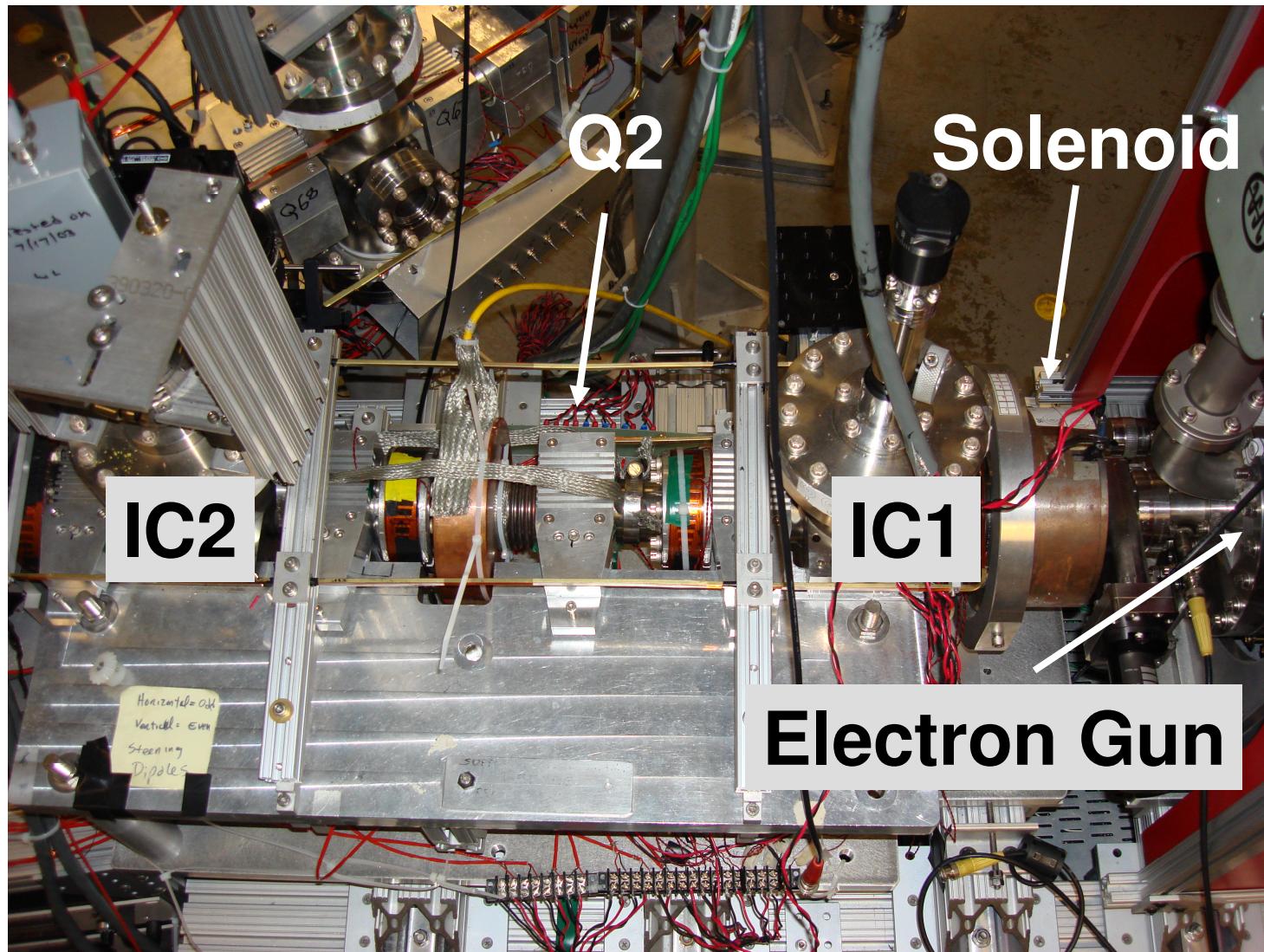
# Magnets: Introduction

- Magnets are key components of all accelerators
- Magnet modeling has several stages:
  1. Simple **hardedge** models for optics design (**energy** and **type** of charged particle are main considerations)
  2. Computer calculations
  3. Mechanical/electrical design and construction
  4. Magnet measurement:  
**field/gradient** profile and/or **multipole** measurement
  5. Beam testing
- Item 1 requires a **magnet strength per amp or volt**, and an **effective length**. Items 2 and 4 yield actual values.
- Measurement devices: gaussmeters (e.g. Hall-effect), rotating coils, taut wire techniques, etc.
- **Computer codes**: OPERA3D/TOSCA, MERMAID, AMPERE, MAG-LI 2

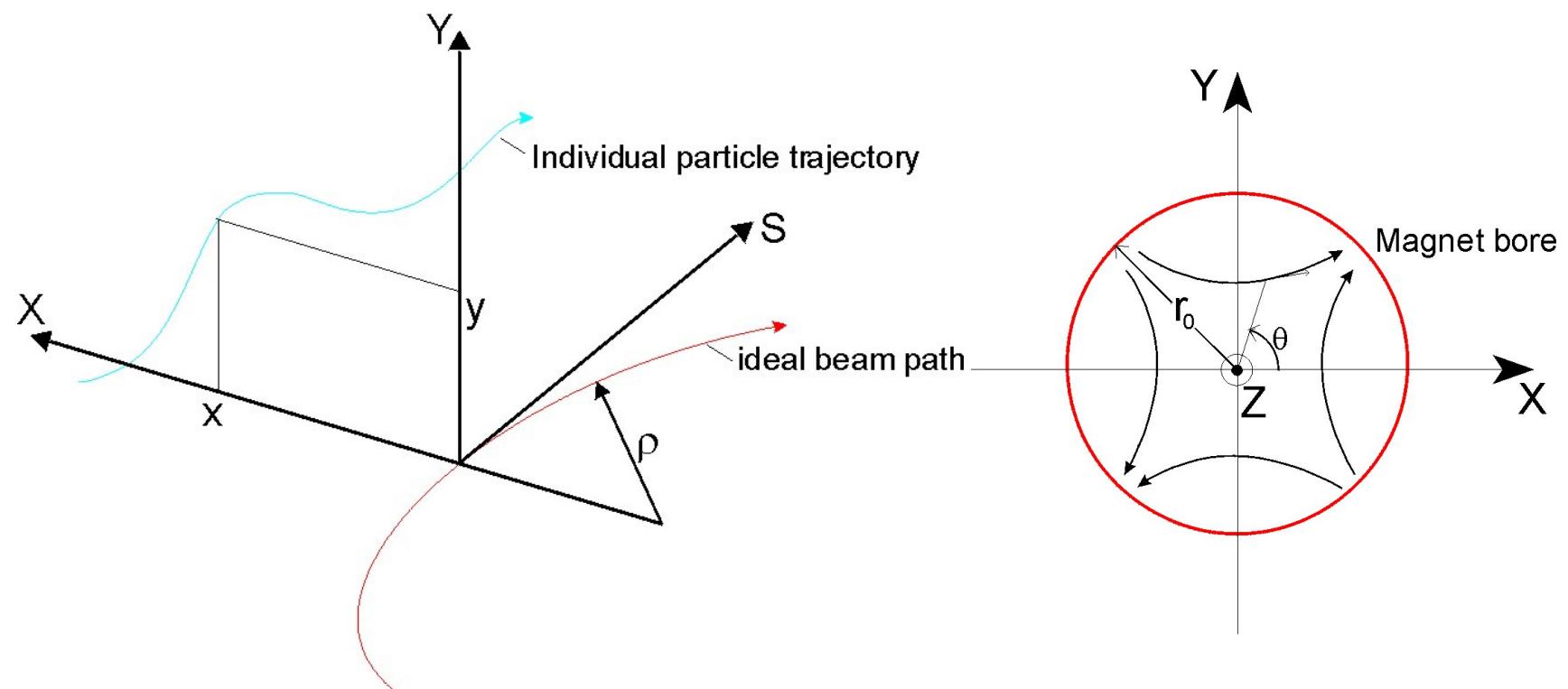
# Magnets: Introduction



# Magnets in UMER: Matching Section



# Coordinate Systems and Notation



Bending dipoles define **reference trajectory**.

$$\gamma mv^2/\rho = qvB \rightarrow B\rho = p/q: \text{Magnetic Rigidity}$$

## Defined as:

$$B\rho = \frac{p}{q}, \quad p = \gamma m \beta c$$

For relativistic e-:

$$B\rho = \frac{p}{e} \cong 0.3 \text{ pc}$$

# Bending:

$$d\theta = ds/\rho(s), \text{ so}$$

$$\theta_2 - \theta_1 = \int_{s_1}^{s_2} \frac{ds}{\rho(s)} \cong \frac{3.0}{pc} \int_{s_1}^{s_2} B(s) ds$$

## Focusing:

$$x''(z) + \kappa_{0x} x(z) = 0, \quad y''(z) + \kappa_{0y} y(z) = 0.$$

- Quadrupole:  $\kappa_{0x} = -\kappa_{0y} = \frac{g_0}{(B\rho)}$
  - Solenoid:  $\kappa_0 = \frac{B_z^2}{4(B\rho)^2}$   $r''(z) + \kappa_0 r(z) = 0$

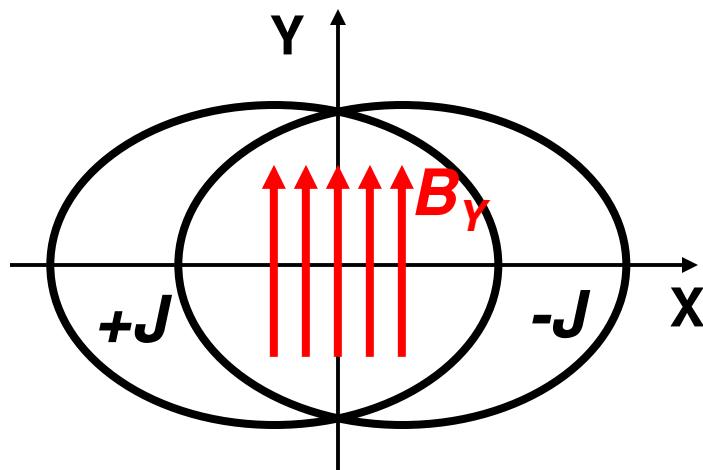
# Magnets: Introduction

Separated Function vs. Combined Function

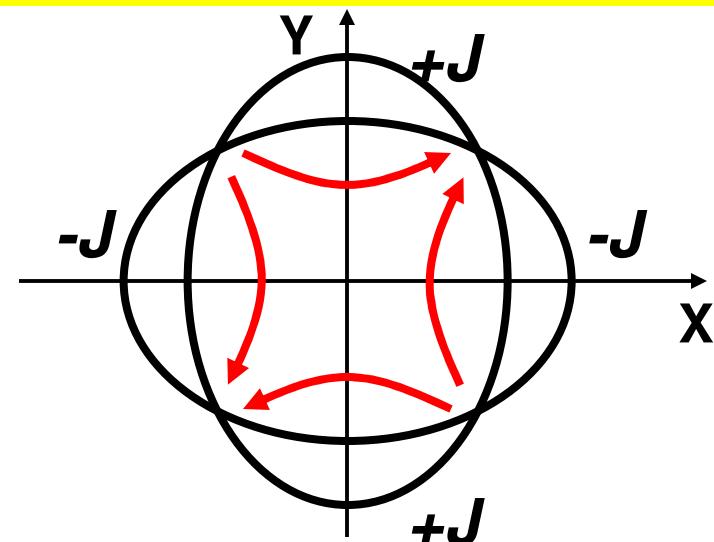
Dipoles, Quadrupoles, Sextupoles, Octupoles

Electrostatic vs. Magnetostatic

Displaced, overlapping (& infinite) solid elliptical cylinders carrying uniform current density generate **pure fields**:



Pure Dipole



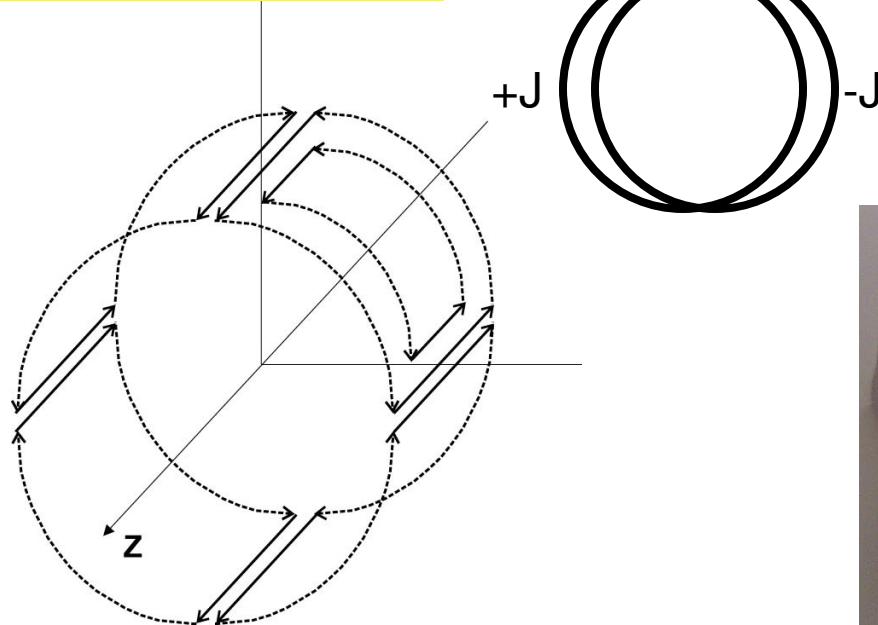
Pure Quadrupole

# UMER PC Dipole and Quadrupole\*

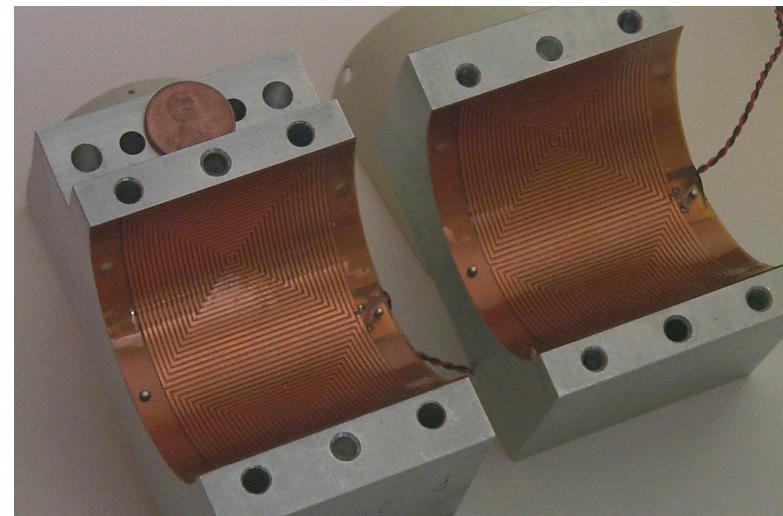
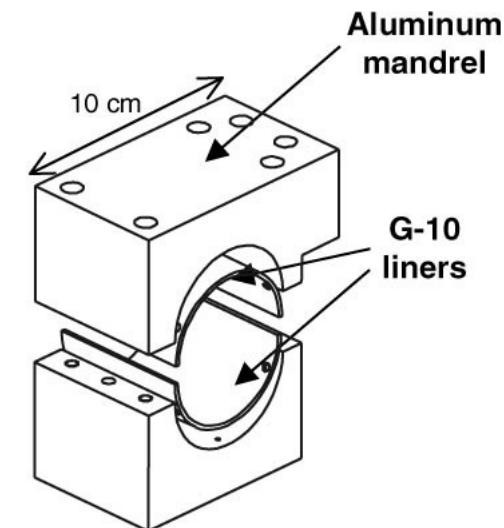
On a circular cylindrical surface,  
we want:  $\int K_z dz \propto \cos n\theta$

$n$ =order of multipole.

Recall...



Only conductors parallel to z-axis contribute to integrated  $B$ -field.



UMER PC quadrupole

\*W.W. Zhang, et al, Phys. Rev. ST Accel. Beams, 3, 122401 (2000).

# Multipole Expansion

## 2D Multipole Expansion:

$$\mathbf{B}(x, y) = \mathbf{B}_y + i\mathbf{B}_x = \sum_{n=1}^{\infty} (b_n + ia_n) \left( \frac{x+iy}{r_0} \right)^{n-1},$$
$$r = \sqrt{x^2+y^2} < r_0, \quad (1)$$

$b_n$  = Normal Component,  
 $a_n$  = Skew Component  
 $r_0$  = Aperture Radius

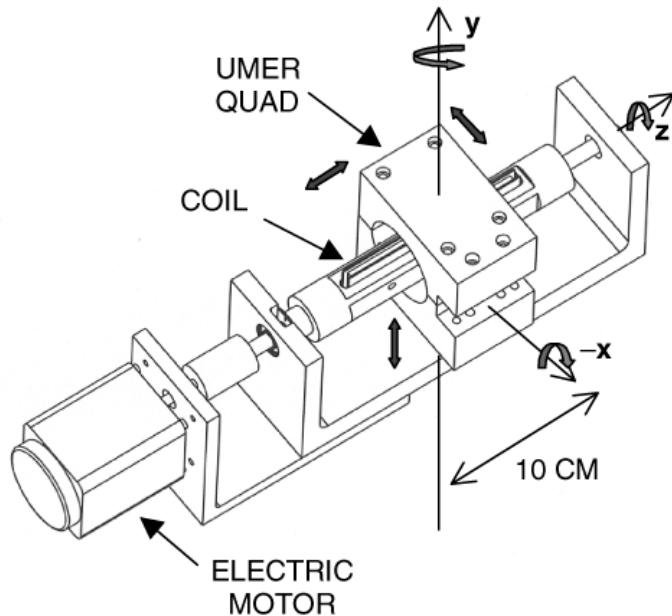
$$B_r(r, \theta) = \sum_{n=1}^{\infty} \left( \frac{r}{r_0} \right)^{n-1} [b_n \sin(n\theta) + a_n \cos(n\theta)],$$
$$B_\theta(r, \theta) = \sum_{n=1}^{\infty} \left( \frac{r}{r_0} \right)^{n-1} [b_n \cos(n\theta) - a_n \sin(n\theta)]. \quad (2)$$

3D Multipole Expansion:  
 $B \rightarrow B^{Int}$

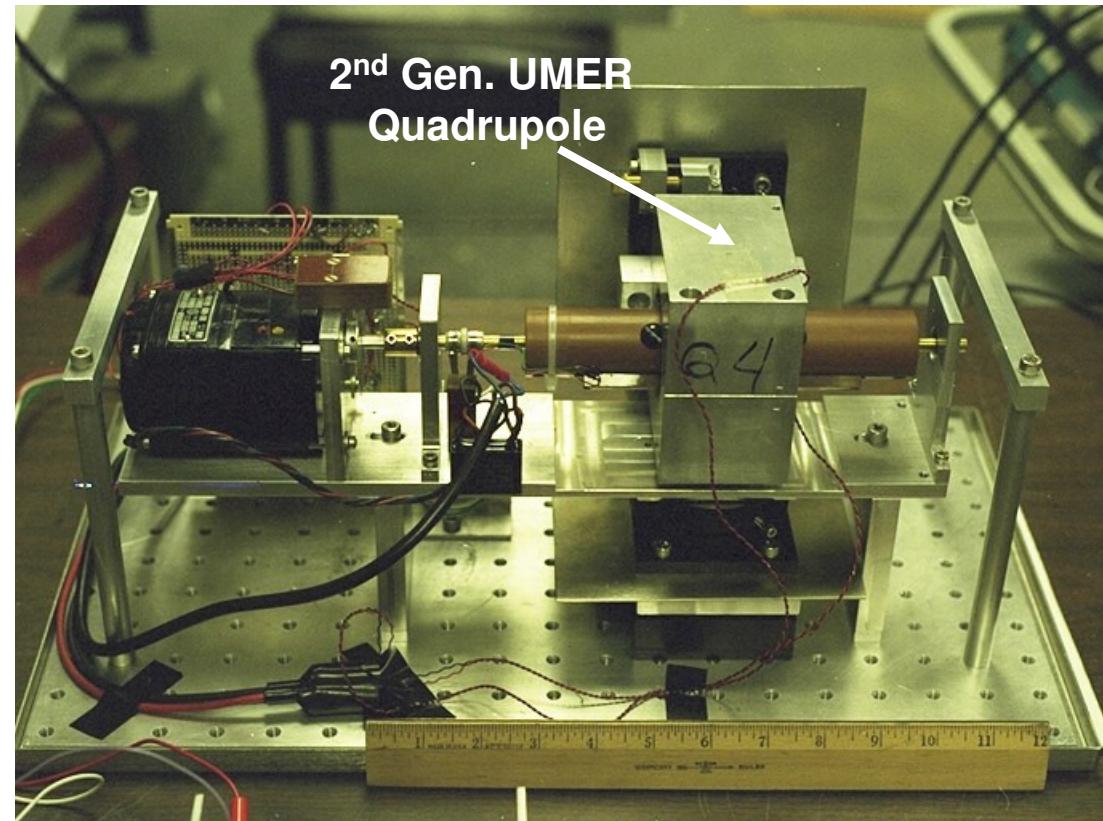
From symmetry, a magnet with **quadrupole symmetry** has only multipoles of the form  $n = 4k+2$  ( $k=0,1,2, \dots$ ), i.e. **quadrupole** ( $n=2$ ), **duodecapole** ( $n=6$ ), 10-pole ( $n=10$ ), etc.

**WE WANT SMALL UNDESIRED MULTIPOLES:**  
typically less than 1 part in  $10^4$

# UMER Rotating Coil\*

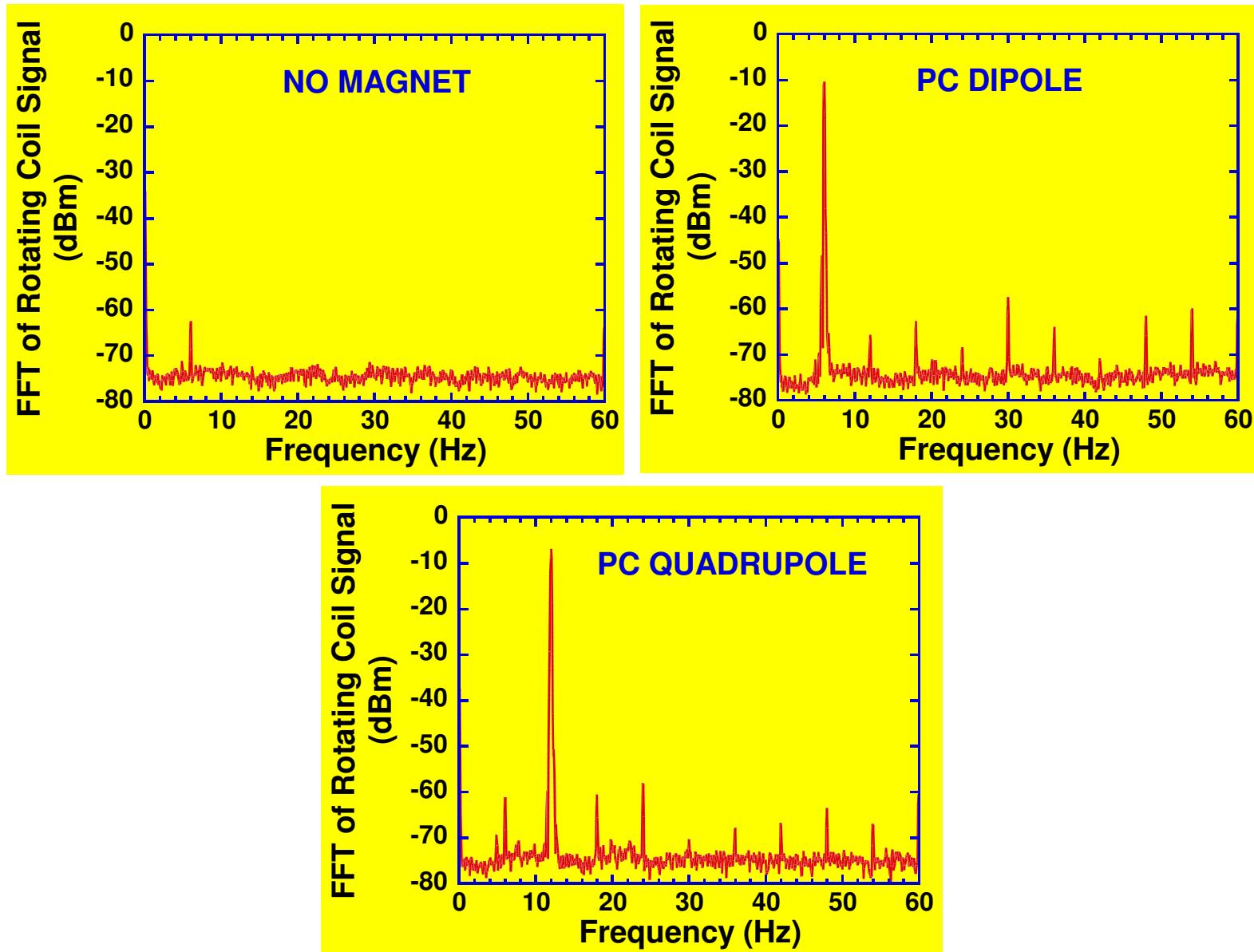


The coil contains ~3000 turns of very fine wire.  
The whole of the rotating coil apparatus is normally enclosed in mu-metal box.

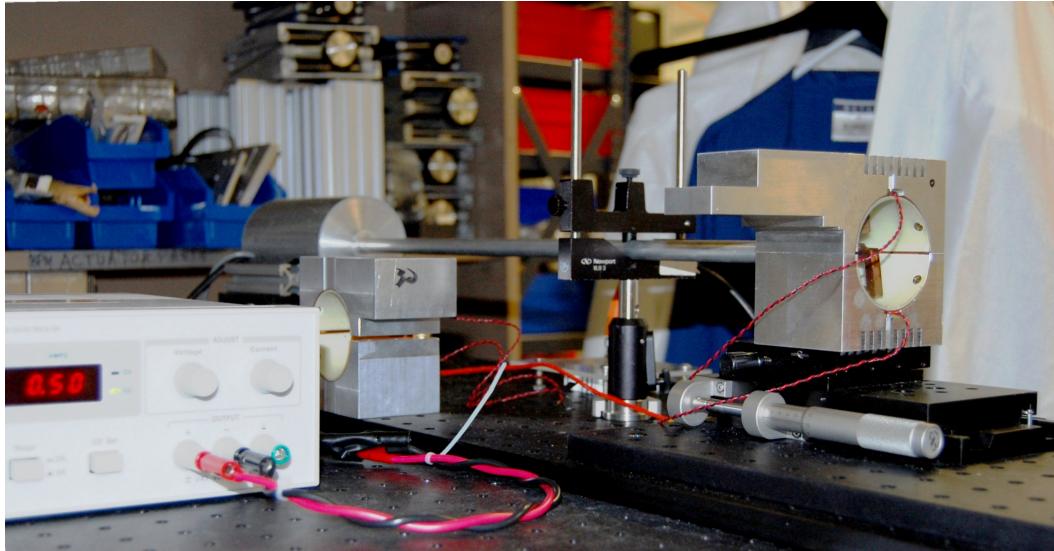


\*W.W. Zhang, et al, Phys, Rev. ST Accel. Beams, 3, 122401 (2000).

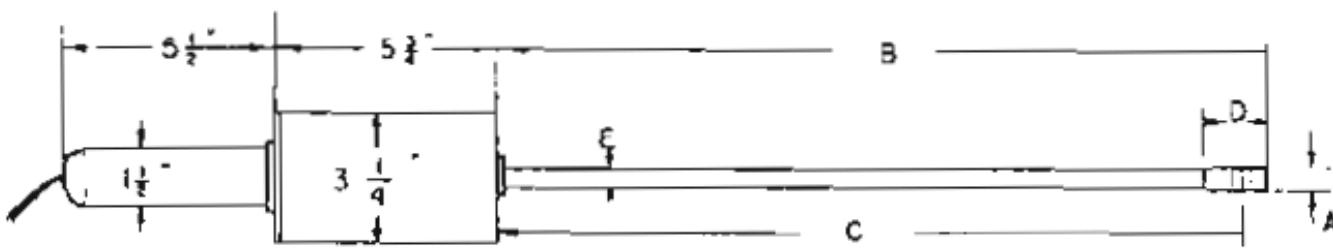
# FFT of Rotating Coil Signal



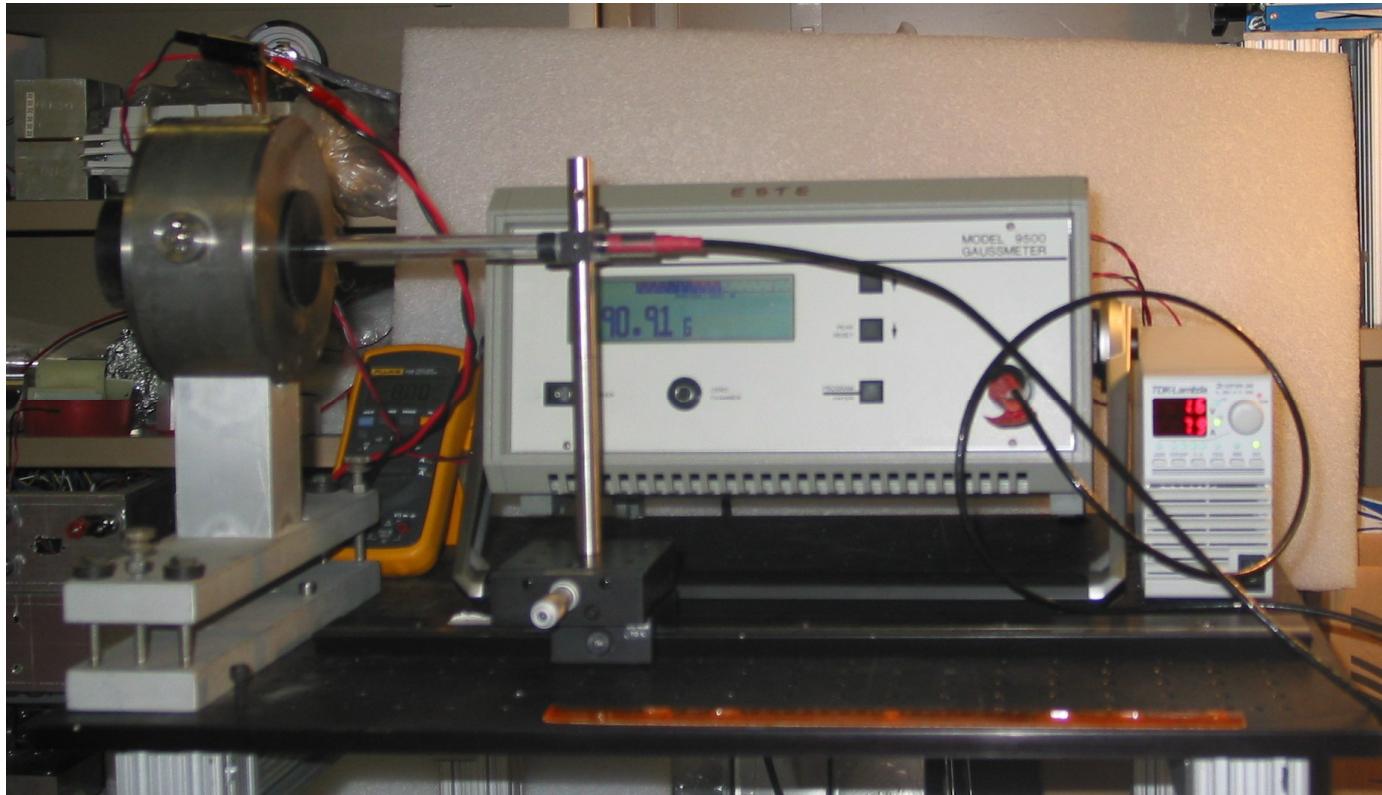
# UMER Simple Rotating Coil



Rawson-Lush rotating coil gaussmeter  
Model 780:  
Tip Diameter. **A**: 6.35 mm  
Probe Length **B**: 50.0 cm  
Length to coil center **C**: 48.9 cm  
Tube Diameter **E**: 6.35 mm



# Short Solenoid: Axial Field Profile Measurement

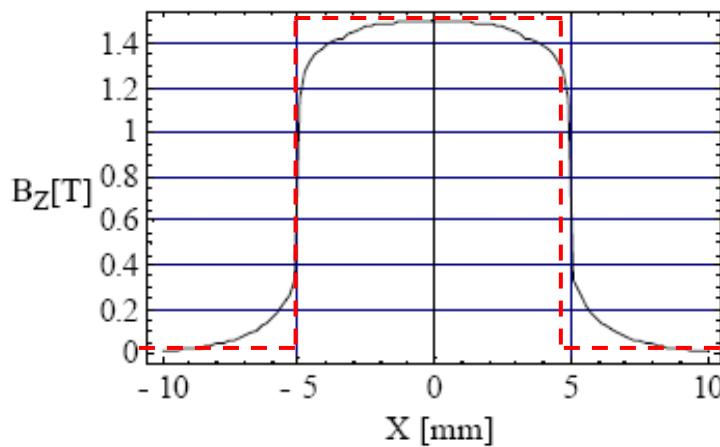
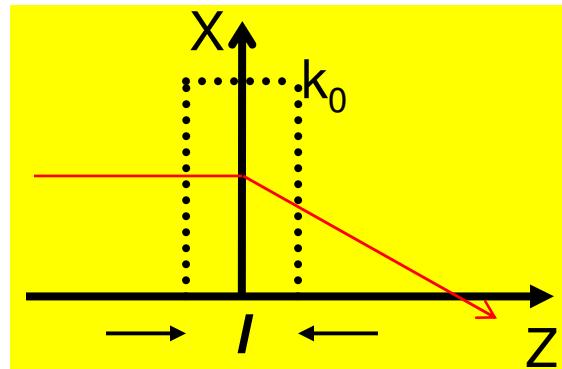
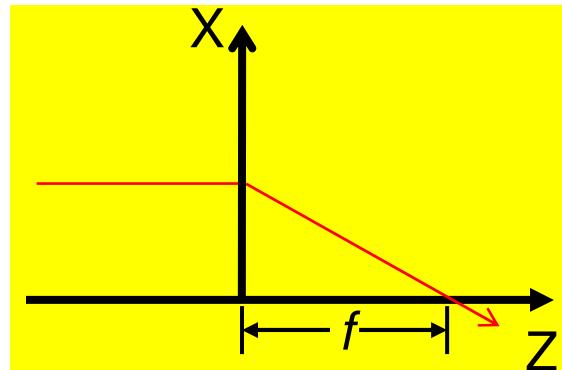


For **axially symmetric  $B$ -fields**, components  $B_z$ ,  $B_r$  can be found at all  $(z, r)$  from knowledge of  $B_z(r=0,z)=B(z)$ , i.e. the **on-axis field profile**:

$$B_r(r,z) = -\frac{r}{2} \frac{\partial B}{\partial z} + \frac{r^3}{16} \frac{\partial^3 B}{\partial z^3} - \dots,$$

$$B_z(r,z) = B - \frac{r^2}{4} \frac{\partial^2 B}{\partial z^2} + \frac{r^4}{64} \frac{\partial^4 B}{\partial z^4} - \dots$$

# Review: Modeling of Lenses



“Point” Lens:

$$x''(z) + \frac{\delta(z)}{f} x(z) = 0$$

Thin Hard-Edge ( $f \gg l$ ):

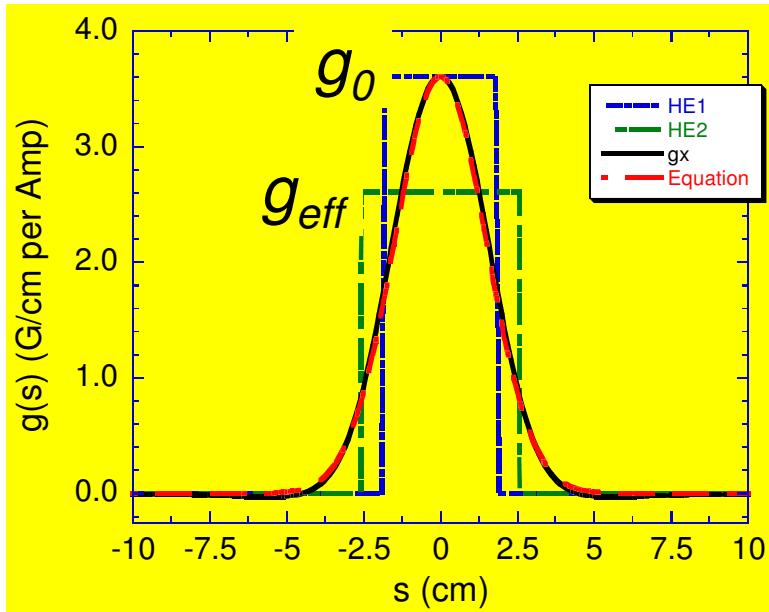
$$x''(z) + \kappa_0 x(z) = 0 \rightarrow \frac{1}{f} = |\kappa_0|$$

Smooth-Profile:

$$x''(z) + \kappa(z)x(z) = 0 \rightarrow \frac{1}{f} = |_{\text{eff}} \kappa_{\text{peak}}$$

$$|_{\text{eff}} = \frac{1}{\kappa_{\text{peak}}} \int_{-z_1}^{z_1} \kappa(z) dz$$

# Effective Length of UMER Quadrupole\*



Red curve is analytical fit to Mag-Li profile (black curve):

$$g(s) = g_0 \exp(-s^2/d^2),$$

$$g_0 = 3.61 \text{ G/cmA}, \quad d = 2.10 \text{ cm}.$$

Standard definition of effective length (which uses hardtop gradient  $g_0$ ) yields

$$l_{eff} = 3.72 \text{ cm}$$

However, the same focal length can be obtained with a wider hardedge model with smaller hardtop gradient  $g_{eff}$ .

For the short UMER quad the correct hardedge model yields

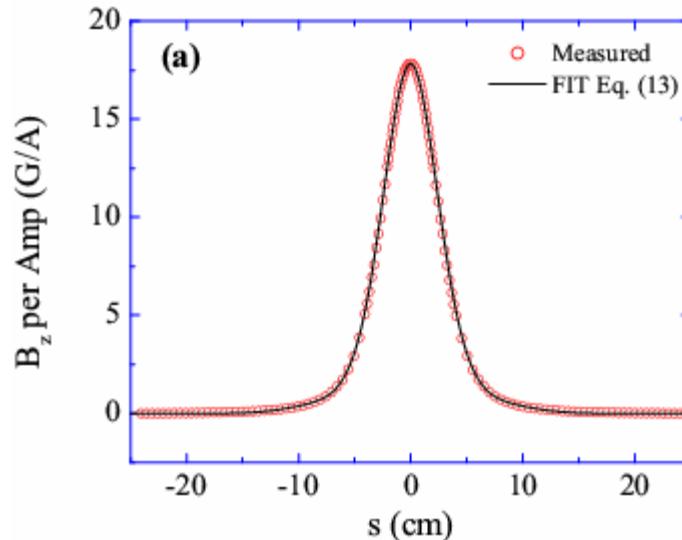
$$l_{eff} = 5.16 \text{ cm}, \quad g_{eff} = 0.72 \times g_0$$

\*S. Bernal, et al, Phys, Rev. ST Accel. Beams, 9, 064202 (2006).

# Effective Length of Short Solenoid\*

UMER Solenoid Profile

$$B_z(0, z) = B_0 \exp(-z^2/d^2) [\operatorname{sech}(z/b) + C_0 \sinh^2(z/b)]$$



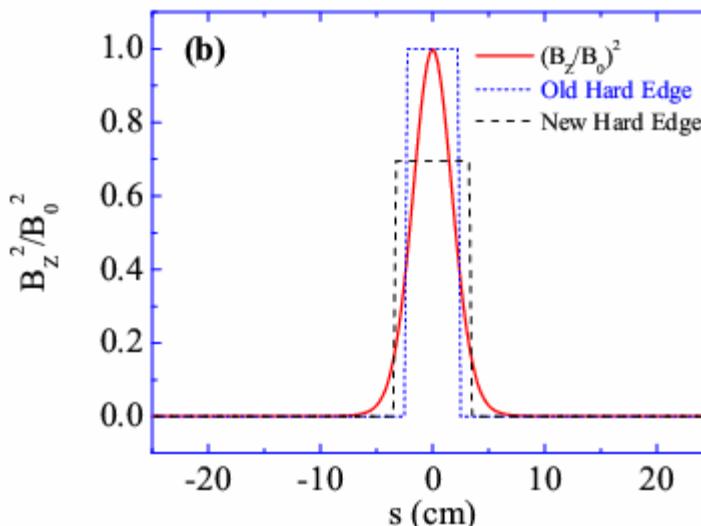
Effective length calculated the standard way is  $l_{\text{eff}} = 4.50$  cm

Similar issues as with the UMER quad...

For UMER short solenoid, new treatment yields

$$l_{\text{eff}}(\text{cm}) = 6.571 \text{ cm} - 0.00029 \times \kappa_{\text{peak}}(\text{m}^{-2}),$$
$$\kappa_{\text{eff}}(\text{m}^{-2}) = 0.6945 \times \kappa_{\text{peak}}(\text{m}^{-2})$$

The effective length has a slight dependence on peak focusing function.



\*S. Bernal, et al, Phys, Rev. ST Accel. Beams, 9, 064202 (2006).

# References

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12. [S. Bernal, et al, Phys. Rev. ST Accel. Beams, 9, 064202 \(2006\)](#).